

# Extending the Inductor Operating Frequency for Optimally-coupled Wireless Power Transfer Systems

Fabian L. Cabrera, Renato S. Feitoza and F. Rangel de Sousa  
fabian.l.c@ieee.org, renato.feitoza@grad.ufsc.br, rangel@ieee.org



Laboratório de Radiofrequência  
Universidade Federal de Santa Catarina

IMOC 2015

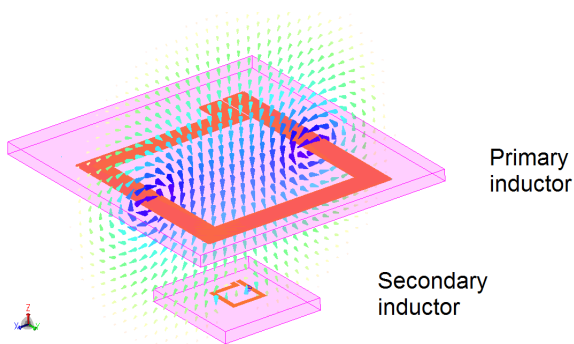


## Inductive links

- ▶ Used to wireless powering IMD (implanted medical devices) and RFID tags.

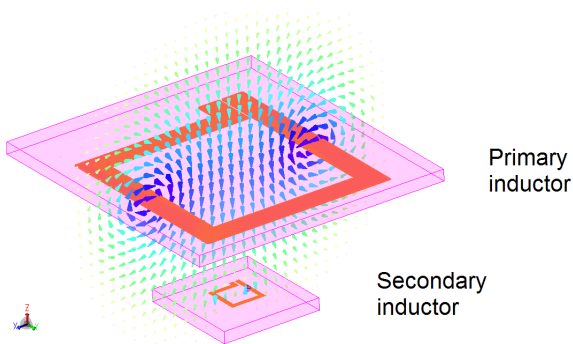
## Inductive links

- ▶ Used to wireless powering IMD (implanted medical devices) and RFID tags.



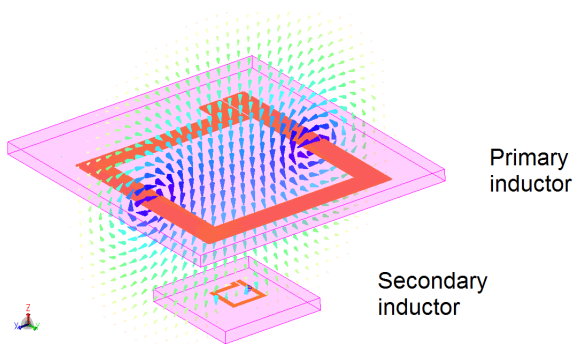
## Inductive links

- ▶ Used to wireless powering IMD (implanted medical devices) and RFID tags.
- ▶ The secondary inductor must be miniaturized.



## Inductive links

- ▶ Used to wireless powering IMD (implanted medical devices) and RFID tags.
- ▶ The secondary inductor must be miniaturized.
- ▶ The primary size constraints are more relaxed.





Efficiency must be maximized

$$\frac{1}{\eta} = \frac{1}{k^2} \cdot \frac{1}{Q_1} \cdot \frac{1}{Q_2} \cdot \underbrace{\left( p + 2 + \frac{1}{p} \right) + p + 1}$$



Efficiency must be maximized

$$\frac{1}{\eta} = \frac{1}{k^2} \cdot \frac{1}{Q_1} \cdot \frac{1}{Q_2} \cdot \underbrace{\left( p + 2 + \frac{1}{p} \right) + p + 1}$$

► Coupling factor squared



Efficiency must be maximized

$$\frac{1}{\eta} = \frac{1}{k^2} \cdot \frac{1}{Q_1} \cdot \frac{1}{Q_2} \cdot \underbrace{\left( p + 2 + \frac{1}{p} \right) + p + 1}$$

- ▶ Coupling factor squared
- ▶ **First Inductor quality factor**





## Efficiency must be maximized

$$\frac{1}{\eta} = \frac{1}{k^2} \cdot \frac{1}{Q_1} \cdot \frac{1}{Q_2} \cdot \underbrace{\left( p + 2 + \frac{1}{p} \right) + p + 1}$$

- ▶ Coupling factor squared
- ▶ First Inductor quality factor
- ▶ **Second Inductor quality factor**



## Efficiency must be maximized

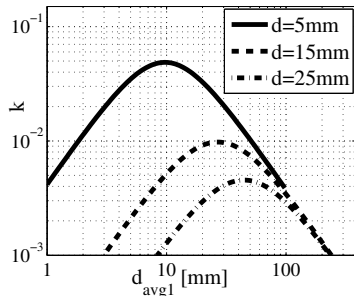
$$\frac{1}{\eta} = \frac{1}{k^2} \cdot \frac{1}{Q_1} \cdot \frac{1}{Q_2} \cdot \underbrace{\left( p + 2 + \frac{1}{p} \right) + p + 1}$$

- ▶ Coupling factor squared
- ▶ First Inductor quality factor
- ▶ Second Inductor quality factor
- ▶ Load matching dependence

$$k = M / \sqrt{L_1 L_2}$$

$$M = \mu \sqrt{\frac{d_{avg1} d_{avg2}}{\pi}} \left[ \left( \frac{2}{\gamma} - \gamma \right) K(\gamma) - \frac{2}{\gamma} E(\gamma) \right] \quad (1)$$

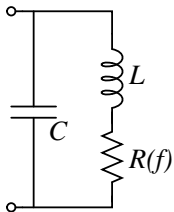
$$\gamma = \sqrt{\frac{4d_{avg1}d_{avg2}}{(d_{avg1} + d_{avg2})^2 + \pi d^2}}, \quad (2)$$

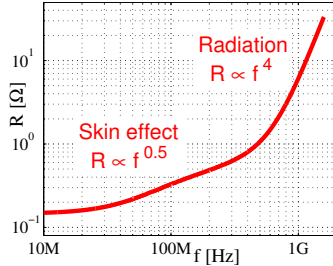
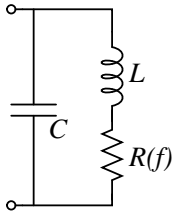


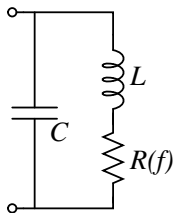
Magnetic coupling factor when  $d_{avg2} = 4$  mm.



# Quality factor model

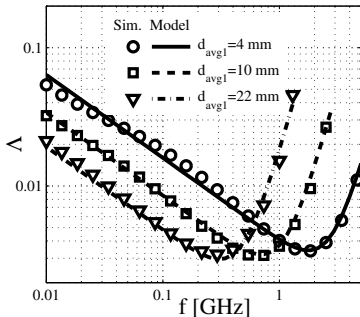
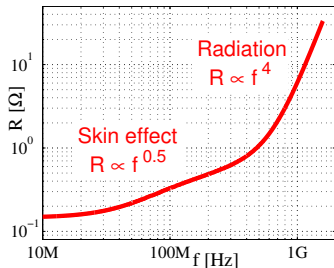






Loss factor

$$\Lambda = \frac{1}{Q} = \frac{R}{2\pi f L}$$





## To maximize efficiency:

- ▶  $k$  must be maximized, this leads to a primary inductor bigger than the secondary.



## To maximize efficiency:

- ▶  $k$  must be maximized, this leads to a primary inductor bigger than the secondary.
- ▶ Operating frequency is then limited by the biggest inductor.





## To maximize efficiency:

- ▶  $k$  must be maximized, this leads to a primary inductor bigger than the secondary.
- ▶ Operating frequency is then limited by the biggest inductor.
- ▶ Therefore, the smaller inductor does not operate in its optimal frequency.

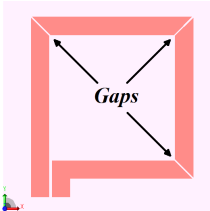


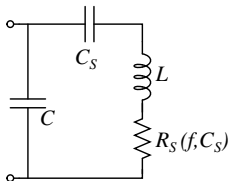
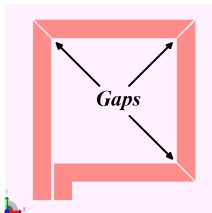
## To maximize efficiency:

- ▶  $k$  must be maximized, this leads to a primary inductor bigger than the secondary.
- ▶ Operating frequency is then limited by the biggest inductor.
- ▶ Therefore, the smaller inductor does not operate in its optimal frequency.
- ▶ We can extend the operating frequency of the link using a segmented inductor.



# Segmented inductor



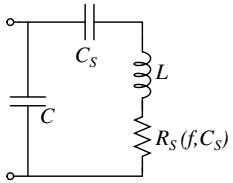
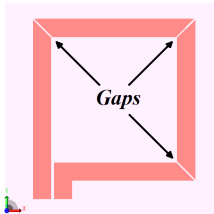


$$C_s = \frac{C_G + C_D}{N - 1}$$

$C_G$  Gap capacitance

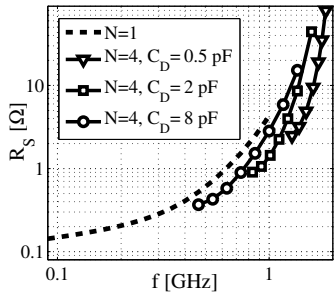
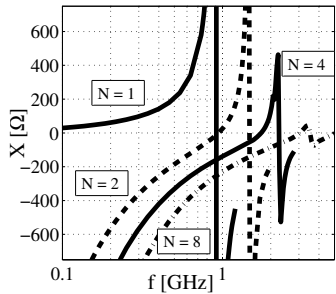
$C_D$  Discrete capacitor

$N$  Number of segments



$$C_S = \frac{C_G + C_D}{N - 1}$$

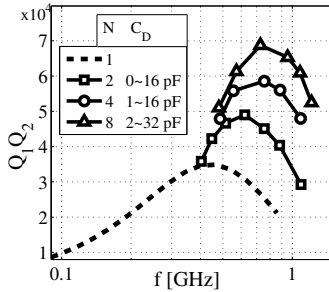
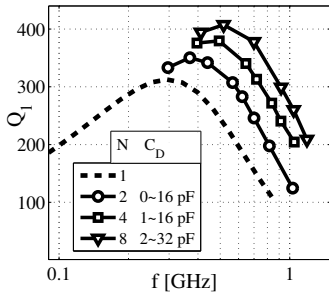
$C_G$  Gap capacitance  
 $C_D$  Discrete capacitor  
 $N$  Number of segments

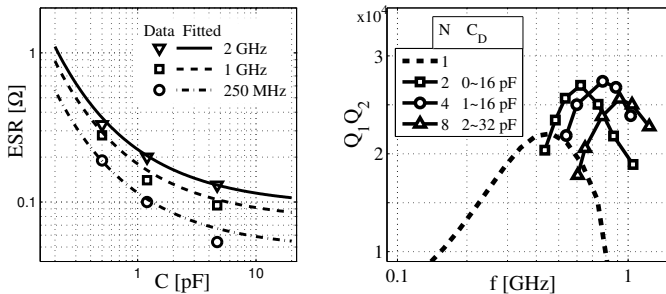


(a) Equivalent reactance when  $C_D=0$ . (b) Segmented inductor losses.



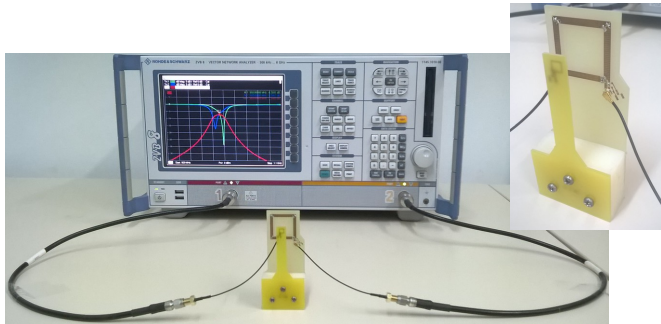
# Segmented inductor quality factor





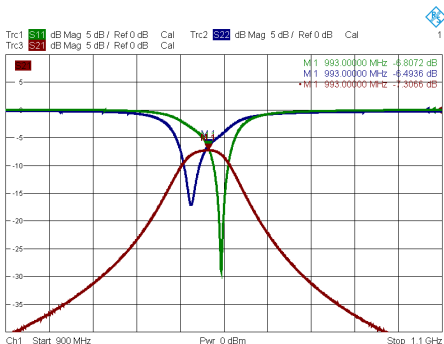
(a) Equivalent series resistance for discrete capacitors. (b) Quality factors product accounting the capacitors ESR.

- Performance is no longer improved for higher values of  $N$  because of the capacitor losses.



$d_{avg2}$ [mm]	$d_{avg1}$ [mm]	$N$	$C_D$ [pF]	$d$ [mm]
4	22	4	3	15





$N$	$C_D$ [pF]	$\eta_{max}$ [%]	$f_{\eta_{max}}$ [MHz]	
1	—	30	415	Meas. [3]
4	3	38	735	Sim.
4	1.5	37	990	Sim.
4	1.5	30	980	Meas.

[3] Fabian L. Cabrera and F. Rangel de Sousa, “Optimal Design of Energy Efficient Inductive Links for Powering Implanted Devices,” in BioWireleSS 2014.



## Conclusions:

- ▶ The operating frequency of an optimally-coupled inductive link was extended from 415MHz to 980 MHz.



## Conclusions:

- ▶ The operating frequency of an optimally-coupled inductive link was extended from 415MHz to 980 MHz.
- ▶ The extension of the operating frequency was achieved by dividing the primary inductor into four segments.



## Conclusions:

- ▶ The operating frequency of an optimally-coupled inductive link was extended from 415MHz to 980 MHz.
- ▶ The extension of the operating frequency was achieved by dividing the primary inductor into four segments.
- ▶ The technique presented offers potential improvements on the link efficiency, however that improvements are limited by the capacitor losses.



## Conclusions:

- ▶ The operating frequency of an optimally-coupled inductive link was extended from 415MHz to 980 MHz.
- ▶ The extension of the operating frequency was achieved by dividing the primary inductor into four segments.
- ▶ The technique presented offers potential improvements on the link efficiency, however that improvements are limited by the capacitor losses.
- ▶ The extension of the primary inductor frequency offers flexibility to the inductive link design.